

CORRECTED VERSION

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
23 December 1999 (23.12.1999)

PCT

(10) International Publication Number  
WO 99/66229 A3

(51) International Patent Classification<sup>6</sup>: F16H 3/091,  
63/14, 55/17

(21) International Application Number: PCT/US99/13350

(22) International Filing Date: 14 June 1999 (14.06.1999)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
09/098,014 15 June 1998 (15.06.1998) US

(71) Applicant: CUSTOM CHROME, INC. [US/US]; 16100  
Jacqueline Court, Morgan Hill, CA 95037 (US).

(72) Inventors: NEGHERBON, Matthew, Stephen; 285-A  
Lindo Lane, Morgan Hill, CA 95037 (US). BOSSLER,  
Robert, Burns, Jr.; Apartment J-7, 2408 South Ha-  
cienda Boulevard, Hacienda Heights, CA 91754 (US).  
WILLIAMS, Arthur, Carl; 2616 North Keystone Street,  
Burbank, CA 91504 (US). STERN, Daniel; 6410 Camino  
Verde Drive, San Jose, CA 95119 (US).

(74) Agents: CICCARELLI, Max et al.; Felsman, Bradley,  
Vaden, Gunter & Dillon, L.L.P., Suite 1600, 201 Main  
Street, Fort Worth, TX 76102 (US).

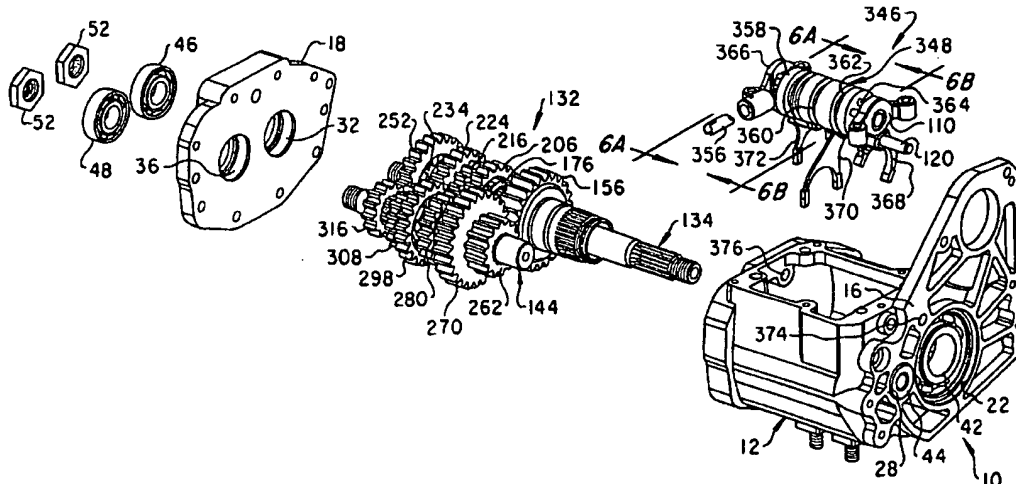
(81) Designated States (*national*): AL, AM, AT, AU, AZ, BA,  
BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES,  
FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE,  
KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG,  
MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE,  
SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, UZ, VN, YU,  
ZW.

(84) Designated States (*regional*): ARIPO patent (GH, GM,  
KE, LS, MW, SD, SL, SZ, UG, ZW), Eurasian patent (AM,  
AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT,  
BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC,  
NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA,  
GN, GW, ML, MR, NE, SN, TD, TG).

Published:  
— With international search report.

[Continued on next page]

(54) Title: SIX SPEED OVERDRIVE MOTORCYCLE TRANSMISSION



(57) Abstract: A six speed gear assembly is having a mainshaft, countershaft, mainshaft 1st-6th gears, countershaft 1st-6th gears, and 4th/6th gear shift member. A shifting assembly with a shifter cam having uniformly distributed and uniformly shaped detents that are engaged by the shift cam follower. The six speed gear assembly has modes of operation corresponding to six speeds (1st through 6th) and a neutral position. The sixth speed is an overdrive speed (the output from the transmission turns faster than the input to the transmission), while the first through fifth speeds correspond to conventional gear ratios. The six speed gear assembly and the shifting assembly fit within the transmission case of a Big Twin five speed transmission without the need to modify the transmission case. This allows the conversion of a Big Twin five speed transmission into a six speed transmission without removal or replacement of the transmission case and by replacing a minimal number of components.

WO 99/66229 A3



(88) Date of publication of the international search report:  
11 May 2000

(15) Information about Correction:  
see PCT Gazette No. 26/2001 of 28 June 2001, Section II

(48) Date of publication of this corrected version:  
28 June 2001

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*

## SIX SPEED OVERDRIVE MOTORCYCLE TRANSMISSION

DescriptionTechnical Field

This invention relates in general to motorcycle transmissions and in particular to motorcycle transmissions used on Harley-Davidson® Big Twin motorcycles, which have transmission cases that are characterized by being separate from the engine case and having concentric input and output members disposed on the same side of the transmission.

Background Art

Different manufacturers of motorcycles, and different models from the same manufacturer, use different types and configurations of transmissions. The particular type of transmission used depends, amongst other things, on the history of the particular motorcycle, its intended uses, and its physical characteristics. Harley-Davidson® Big Twin motorcycles have a rather unique transmission in that the transmission case is truly separate from the engine case.

A brief description of the Harley-Davidson® Big Twin five speed transmission will help in understanding the present invention.

Referring first to Figure 1A, the major components of a prior art Big Twin five speed transmission are shown in a partially exploded view. Many of the smaller components, which are well known to those skilled in the art, are not shown for clarity. A Big Twin five speed transmission case 10 is shown. The particular transmission case depicted as 10 is for Softail® models from 1989 to at least 1998; however, the invention is equally applicable to transmission cases for all other Softail® vintages and the other Big Twins (e.g. Softail®, Dyna®, FXR, and FLT), due to the large similarity. The transmission cases for the various Big Twins vary only in a few external dimensions that relate mainly to the attachment of the transmission case to, and fitment of the transmission case around, the particular frame and surrounding components of the particular Big Twin. The inner cavity and components of the transmissions for the various Big Twins are otherwise almost identical.

Transmission case 10 has a housing 12 with a central portion 14, left side

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wall 16, and a removable right side wall (or trapdoor) 18 defining a cavity 20. Recess 22 is located in left side wall 16 for receiving the left mainshaft case bearing 42, and recess 28 is located adjacent recess 22 for receiving the left countershaft case bearing 44. Recess 30 is located in trapdoor 18 for receiving the right mainshaft trapdoor bearing 46, and recess 36 is located adjacent recess 30 for receiving the right countershaft trapdoor bearing 48.

Referring still to Figure 1A, five speed gear set 60 comprises mainshaft (or driveshaft) 62, countershaft 64, mainshaft 5th gear (also referred to as driveshaft drive gear or driveshaft output gear) 66, mainshaft 2nd gear 68, mainshaft 3rd gear 70, mainshaft 1st gear 72, mainshaft 4th gear 74, countershaft 5th gear 76, countershaft 2nd gear 78, countershaft 3rd gear 80, countershaft 1st gear 82, and countershaft 4th gear 84. Some of the components of five speed gear set 60 are not shown or are hidden from view; for example, split case bearings, retaining rings, thrust washers, and spacers.

To install five speed gear set 60 into transmission case 10, mainshaft 62 and countershaft 64 are first secured to trapdoor 18 by means of hex nuts 52. Right mainshaft trapdoor bearing 46 supports the right end of mainshaft 62. Right countershaft trapdoor bearing 48 supports the right end of countershaft 64. The gears and related hardware (split case bearings, retaining rings, thrust washers, and spacers) are then positioned about the mainshaft 62 and countershaft 64. Then, trapdoor 18, with five speed gear set 60 secured thereto, is fastened to the housing (by conventional fasteners which are not shown).

When five speed gear set 60 is installed into transmission case 10, the outer bearing surface 86 of mainshaft 5th gear 66 is secured by the left mainshaft case bearing 42. Mainshaft 5th gear bearings 50 (not shown in Figure 1A, but well known in the industry) keep mainshaft 62 concentric with mainshaft 5th gear 66. The outer splined portion 88 of the mainshaft 5th gear 66 and the left end of mainshaft 62 protrude outside of transmission case 10. The left end of countershaft 64 is received by left countershaft case bearing 44.

Referring still to Figure 1A, shifting assembly 94 is shown. Shifting assembly 94 comprises shifter cam 96 supported by left and right shift cam support towers 110 and 112. The shift grooves 98, 100, 102 are shown, but, for convenience,

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have not been accurately depicted because they are well known. Left and right shift cam support towers 110 and 112 are connected to the top of housing 12. Shifter forks 114, 116, and 118 are supported by shift fork shaft 120, which is in turn supported by shift fork shaft support holes 122 and 124.

5           In operation, when the shifter shaft (not shown) rotates in response to the rider operating the shift lever (not shown), the shifter pawl (not shown) acts against the shift pins 104 causing shifter cam 96 to rotate. The interaction of shift cam follower 108 and detents 106 biases the shifter cam 96 to predetermined angular positions of the shifter cam 96. The rotation of shifter cam 96 causes one or more  
10 of shifter forks 114, 116, 118 to move axially along shift fork shaft 120, in turn causing the appropriate gear members to move axially along either mainshaft 62 or countershaft 64, causing a change in the gear ratio.

Referring now to Figure 1B, a schematic horizontal cross section of empty transmission case 10 is shown to better illustrate the location of, and respective  
15 distances between, bearings 42, 44, 46, and 48. Left countershaft case bearing 44 is pressed into recess (or hole) 28. Left mainshaft case bearing 42 is held in position within recess 22 by bearing shoulder 24 and by a snap ring (not shown) held by snap ring groove 26. Right countershaft trapdoor bearing 48 is held in position within recess 36 by bearing shoulder 38 and by a snap ring (not shown) held by  
20 snap ring groove 40. Right mainshaft trapdoor bearing 46 is held in position within recess 30 by bearing shoulder 32 and by a snap ring (not shown) held by snap ring groove 34.

The distance from the outside of bearing shoulder 24 (i.e. the inside of left mainshaft case bearing 42) to the outside of bearing shoulder 32 (i.e. the inside of  
25 right mainshaft trapdoor bearing 46) is 5.97 inches. This distance is characteristic of Big Twin five speed transmissions. Any mainshaft that is to be used in one of these transmission cases without need to modify the transmission case or the trapdoor, must have bearing surfaces that register with left mainshaft case bearing 42 and right mainshaft trapdoor bearing 46 that are separated by 5.97 inches. The  
30 same is true of any countershaft that is to be used in one of these transmission cases without need to modify the transmission case or the trapdoor, in that such a countershaft must have bearing surfaces that register with a left countershaft case

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bearing 44 and a right countershaft trapdoor bearing 48 that are separated by 6.10 inches (as measured from the inside of left countershaft case bearing 44 to the inside of right countershaft trapdoor bearing 48).

5 Referring now again to Figure 1A, when assembled, five speed gear set 60 is located inside housing 12, with trapdoor 18 fastened to the right side of housing 12, with shifting assembly 94 fastened to the top of housing 12, and the appropriate covers (for example, transmission top cover and transmission end cover) and other components in place.

10 There are few modern motorcycles that have transmission cases separate from the engine case. BMW motorcycles, for example, have transmission cases that are bolted to the engine case, but that can be unbolted during service. Historically, more motorcycles had separate engine and transmission cases. The modern trend, for motorcycles other than Big Twins, seems to be toward unitary engine and transmission cases.

15 Motorcycle transmission cases, in general, are designed to be as small as possible because of weight and size considerations. This is especially true when the transmission case is separate and therefore already heavier than if it were combined with the engine case. Thus, the cavity inside the transmission case is generally small.

20 Another reason why the transmissions for Harley-Davidson® Big Twin motorcycles is unique is that the large amount of torque generated by the engines available on those motorcycles has, historically, lead to little attention being given to optimizing the gearing. Harley-Davidson made some improvements, for example, by introducing 4 speed transmissions in the 1930's and then introducing 5 speed  
25 transmissions in the 1980's. Adding additional gears allows one to take better advantage of narrower power bands. However, because Harley-Davidson® Big Twin motorcycles have so much torque and such a wide power band, adding additional gears has not been a high priority. In racing motorcycles, adding additional gears to take better advantage of the narrower power bands on racing-tuned engines is  
30 common, but that is not the case on Big Twins.

On Big Twins, the more prevalent concern is to lower the engine r.p.m. at cruising speed. Often, this is done by replacing the stock rear pulley with a smaller

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one. This has the effect of increasing the motorcycle speed for any given engine r.p.m., or conversely, to reduce the engine r.p.m. for any given speed. Although reducing the size of the rear pulley lowers cruising r.p.m. (or, conversely, increases cruising speed), it effects performance at all the gears.

5 Custom, replacement gear sets are also available that modify some of the stock gear ratios. For example, the assignee of this patent, Custom Chrome, offers its RevTech® gear sets for 5 speed Big Twin transmissions in either the stock 3.24:1 or close-ratio 2.94:1 first gears. However, because of size limitations of the transmission case cavity, the changes that have been possible through replacement  
10 gear sets have been minor.

Complete custom transmissions (often larger than stock) are also available if more significant modifications are required than are permitted by the size limitations of the transmission case cavity. However, replacing a transmission case can take in excess of 8 hours if performed by a trained mechanic. If a less-trained, weekend  
15 motorcycle-enthusiast would undertake such a task, it could probably mean having a dismantled motorcycle in the garage or shop for several days.

Thus, the need exists for a method or apparatus for providing low cruising r.p.m. for Big Twin motorcycles without affecting the other transmission characteristics.

20 The need also exists for increasing top-end speed of Big Twin motorcycles without affecting the other transmission characteristics.

The need also exists for gear configurations that allow a more compact arrangement of gears inside a Big Twin transmission.

The need also exists for a gear set that is stronger and with a longer life.

25 The need also exists for Big Twin transmissions in which the shift pawl can be adjusted when the gears are in more than one configuration (i.e. other than in third gear).

The need also exists for Big Twin transmissions that provide smoother, more uniform shifting, with the same lever throw in every gear.

30 The need also exists for a method and apparatus for fulfilling the above needs that is not detectable from a visual inspection of the assembled motorcycle.

The need also exists for a method and apparatus for fulfilling the above needs

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with a minimum amount of work and expense on the part of the motorcycle owner or mechanic.

Disclosure of Invention

5 It is the general objective of the invention to provide a method and apparatus for providing low cruising r.p.m. for Big Twin motorcycles without affecting the other transmission characteristics.

It is another objective of the invention to provide a method and apparatus for increasing the speed of Big Twin motorcycles in top gear while keeping the engine r.p.m. in the optimum operating range.

10 It is yet another objective of the invention to provide gear configurations that allow a more compact arrangement of gears inside a Big Twin transmission.

It is another objective of the invention to provide a gear set that is stronger and with a longer life.

15 Another objective of the invention is to provide Big Twin transmissions in which the shift pawl can be adjusted when the gears are in more than one configuration (i.e. other than in third gear).

Yet another objective of the invention is to provide a Big Twin transmission with smoother, more uniform shifting, with the same lever throw in every gear.

20 Yet another objective of the invention is to provide a method and apparatus for fulfilling the above objectives in a manner that is not detectable from a visual inspection of the assembled motorcycle.

Another objective of the invention is to provide a method and apparatus for fulfilling the above objectives with a minimum amount of work and expense on the part of the motorcycle owner or mechanic.

25 The above as well as additional objectives are achieved as is now described. A six speed gear assembly is provided having a mainshaft, countershaft, mainshaft 1st-6th gears, countershaft 1st-6th gears, and 4th/6th gear shift member. A shifting assembly is also provided with a shifter cam having uniformly distributed and uniformly shaped detents that are engaged by the shift cam follower. The six speed  
30 gear assembly has modes of operation corresponding to six speeds (1st through 6th) and a neutral position. The sixth speed is an overdrive speed (the output from the transmission turns faster than the input to the transmission), while the first through



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fifth speeds correspond to conventional gear ratios.

The six speed gear assembly and the shifting assembly fit within the original equipment Harley-Davidson® Big Twin five speed transmission without the need to modify the transmission case. This allows the conversion of a Big Twin five speed  
5 transmission into a six speed transmission without removal or replacement of the transmission case and by replacing a minimal number of components.

The above as well as additional objectives, features, and advantages will become apparent in the following description.

#### Brief Description of Drawings

10 Figure 1A is an exploded view of the major components of a prior-art Harley-Davidson® Big Twin five speed transmission.

Figure 1B is a schematic horizontal cross section of the prior-art transmission case of Figure 1A, and additionally showing the case and trapdoor bearings.

15 Figure 2 is an exploded view of a Big Twin transmission case and the six speed gear and shifting assemblies of the present invention.

Figure 3 is an exploded view of the six speed gear assembly of the present invention.

Figure 4 is a cross sectional view of the six speed gear assembly of the present invention.

20 Figures 5A-5C are views of the mainshaft first gear of the present invention.

Figures 6A-6B are views of the shift cam of the present invention taken along lines 6A-6A and 6B-6B, respectively, in Figure 2.

Figure 6C is a view of the cylindrical surface of the shift cam of the present invention.

25 Figures 7A-7G are views of the six speed gear assembly of the present invention showing the movement of the various members to achieve each of the speed selections.

#### Best Mode for Carrying Out the Invention

30 Figure 2 shows a partially exploded view of the gear assembly and other components of the present invention and how those components can be used to convert the five speed transmission of Figure 1A into a six speed transmission.

Referring next to Figure 2, the six speed gear and shifting assemblies of the

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present invention are shown in a partially exploded view together with a five speed transmission case. The transmission case 10 of Figure 2 is the same as transmission case 10 of Figure 1A (including housing 12, left side wall 16, and trapdoor 18), and so are the: bearings 42, 44, 46, and 48; recesses 22, 28, 32, 36; hex nuts 52; left shift cam support tower 110; and shift fork shaft 120.

Looking first at the six speed gear set (or assembly) 132, Figure 3 is an exploded view of that gear set 132. Referring primarily to Figures 2 and 3, six speed gear set 132 comprises mainshaft (or driveshaft) 134, countershaft 144, mainshaft 5th gear (also referred to as driveshaft drive gear or driveshaft output gear) 156, mainshaft 1st gear 176, mainshaft 3rd gear 206, mainshaft 2nd gear 216, mainshaft 4th gear 224, 4th/6th gear shift member 234, mainshaft 6th gear (or mainshaft overdrive gear) 252, countershaft 5th gear 262, countershaft 1st gear 270, countershaft 3rd gear 280, countershaft 2nd gear 298, countershaft 4th gear 308, and countershaft 6th gear (or countershaft overdrive gear) 316. Six speed gear set 132 also includes the necessary split case bearings, retaining rings, thrust washers, and spacers, although, for clarity, not all these components are shown.

Figure 4 shows a cross section of six speed gear set 132. Referring now primarily to Figures 3 and 4, mainshaft 134 has splined regions 136a, 136b, and 136c, and bearing regions 138a, 138b, 138c, 138d, and 138e. The gears and shift member and their arrangement on mainshaft 134 is further described below.

Mainshaft 6th gear 252 is freely rotatably supported by split case bearing 322 on bearing region 138a of mainshaft 134. Mainshaft 6th gear 252 has a diametral pitch of 8, 26 teeth, and a face width of 0.531 inches. On the left side 254 of mainshaft 6th gear 252 are dog recesses 256 to receive right dogs 244 (discussed below) of 4th/6th gear shift member 234.

An alternative design for mainshaft 6th gear 176 has 27 teeth with a diametral pitch of 8.

4th/6th gear shift member 234 is rotatably coupled to, and axially movable with respect to, mainshaft 134 by splined region 136a on mainshaft 134 and splines 236 on 4th/6th gear shift member 234. 4th/6th gear shift member 234 is retained, in part, by retaining ring 334a. 4th/6th gear shift member 234 has a left side 238 with left dogs 240 protruding therefrom and a right side 242 with right dogs 244

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protruding therefrom. Fork groove 246 is located between left side 238 and right side 242 of 4th/6th gear shift member 234.

Mainshaft 4th gear 224 is freely rotatably supported by split case bearing 324 on bearing region 138b of mainshaft 134. Mainshaft 4th gear 224 has a diametral pitch of 8, 23 teeth, and a face width of 0.531 inches. On the right side 226 of mainshaft 4th gear 224 are dog recesses 228 to receive left dogs 240 of 4th/6th gear shift member 234.

Mainshaft 2nd gear 216 is rotatably coupled to mainshaft 134 by splined region 136b on mainshaft 134 and splines 218 on mainshaft 2nd gear 216. Mainshaft 2nd gear 216 has a diametral pitch of 8, 18 teeth, and a face width of 0.531 inches.

Mainshaft 3rd gear 206 is freely rotatably supported by split case bearing 326 on bearing region 138c of mainshaft 134. Mainshaft 3rd gear 206 has a diametral pitch of 8, 21 teeth, and a face width of 0.531 inches. On the left side 208 of mainshaft 3rd gear 206 are dog recesses 210 to receive right dogs 194 (discussed below) of mainshaft 1st gear 176.

Mainshaft 1st gear 176 is rotatably coupled to, and axially movable with respect to, mainshaft 134 by splined region 136c on mainshaft 134 and splines 178 on mainshaft 1st gear 176. Mainshaft 1st gear 176 is retained, in part, by retaining ring 334b.

Referring now to primarily to Figures 3, 4, and 5A-5C, mainshaft 1st gear 176 has a central portion 180, a left end portion 182 with a left flange 184 extending radially therefrom, and a right end portion 186 with a right flange 188 extending radially therefrom. About the circumference of mainshaft 1st gear 176 are 14 teeth 190 with a diametral pitch of 7.8154 and a face width of 0.750 inches. Protruding from the left flange 184 are left dogs 192 which extend longitudinally from the left flange and away from central portion 180. Protruding from the right flange 188 are right dogs 194 which extend longitudinally from the right flange and away from central portion 180. Because of the manner in which Figure 4 has been sectioned, dogs 192 and 194 are not cut by the cross section and appear behind the plane of the drawing and, because of their position, appear closer to mainshaft 134. A left annular groove 196 is defined between left flange 184 and gear teeth 190. A right

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annular groove (or fork groove) 198 is defined between right flange 188 and gear teeth 190. Annular grooves 196 and 198 extend to the same depth as the root of teeth 190. Annular grooves 196 and 198 allow mainshaft 1st gear 176 to move axially along mainshaft 134 without interfering with countershaft 1st gear 270.

5           An alternative design for mainshaft 1st gear 176 has 15 teeth with a diametral pitch of 8.466.

Referring now primarily to Figure 3 and 4, mainshaft 5th gear 156 (also referred to as driveshaft drive gear or mainshaft drive gear) comprises a gear portion 158 rigidly connected to an output sprocket mounting member 160. Gear portion 158 has 25 teeth with a diametral pitch of 8 and a face width of 0.857 inches. Mainshaft 5th gear 156 is freely rotatably supported by left mainshaft case bearing 42 which supports the outside bearing surface 162 of mainshaft 5th gear 156. Mainshaft 5th gear bearings 50 are located between the inside of mainshaft 5th gear 156 and mainshaft 134 at bearing surfaces 138d and 138e, and keep mainshaft 134 concentric with mainshaft 5th gear 156.

On the right side 164 of mainshaft 5th gear 156 there is a gear recess 166 of diameter larger than the greatest addendum diameter of mainshaft 1st gear 176. Gear recess 166 is designed to receive the left flange 184, left annular groove 196, and a portion of teeth 190 of mainshaft 1st gear 176. Gear recess 166, which allows part of mainshaft 1st gear 176 (including a portion of teeth 190) to fit inside mainshaft 5th gear 156 greatly reduces the axial space requirement of six speed gear set 132. At the left end 168 of gear recess 136 are dog recesses 170.

Referring still primarily to Figures 3 and 4, countershaft 144 has splined regions 146a, 146b, and 146c, bearing regions 148a, 148b, 148c, and press-fit region 150.

Countershaft 6th gear 316 is rotatably coupled to countershaft 144 by the press-fit connection between press-fit region 150 of countershaft 144, the inside surface 318 of countershaft 6th gear 316, and key 320. Countershaft 6th gear 316 has a diametral pitch of 8, 13 teeth, and a face width of 0.531 inches.

30           An alternative design for countershaft 6th gear 176 has 13 teeth with a diametral pitch of 8.

Countershaft 4th gear 308 is rotatably coupled to countershaft 144 by splined

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region 146a on countershaft 144 and splines 310 on countershaft 4th gear 308. Retaining ring 332a prevents countershaft 4th gear 308 from moving axially to the right of splined region 146a. Countershaft 4th gear 308 has a diametral pitch of 8, 16 teeth, and a face width of 0.531 inches.

5 Countershaft 2nd gear 298 is freely rotatably supported by split case bearing 328 on bearing region 148a of countershaft 144. Countershaft 2nd gear 298 has a diametral pitch of 8, 21 teeth, and a face width of 0.531 inches. On the left side 300 of countershaft 2nd gear 298 are dog recesses 302 to receive right dogs 292 (discussed below) of countershaft 3rd gear 280.

10 Countershaft 3rd gear 280 is rotatably coupled to, and axially movable with respect to, countershaft 144 by splined region 146b on countershaft 144 and splines 282 on countershaft 3rd gear 280. Countershaft 3rd gear 280 is retained, in part, by retaining rings 332b and 332c. Countershaft 3rd gear 280 has a diametral pitch of 8, 18 teeth, and a face width of 0.531 inches. Countershaft 3rd  
15 gear 280 has a right side 290 with right dogs 292 protruding therefrom, a fork groove 284 to the left of the teeth, and a left side 286 with left dogs 288 protruding therefrom. Because of the manner in which Figure 4 has been sectioned, dogs 288 and 292 are not cut by the cross section and appear behind the plane of the drawing and, because of their position, appear closer to countershaft 144.

20 Countershaft 1st gear 270 is freely rotatably supported by split case bearing 330 on bearing region 148b of countershaft 144. Countershaft 1st gear 270 has a diametral pitch of 7.8154, 23 teeth, and a face width of 0.670 inches. On the right side 272 of countershaft 1st gear 270 are dog recesses 274 to receive left dogs 288 of countershaft 3rd gear 280.

25 An alternative design for countershaft 1st gear 176 has 27 teeth with a diametral pitch of 8.466.

Countershaft 5th gear 262 is rotatably coupled to countershaft 144 by splined region 146c on countershaft 144 and splines 264 on countershaft 5th gear 262. Countershaft 5th gear 262 has a diametral pitch of 8, 14 teeth, and a face width of  
30 0.937 inches.

Six speed gear set 132 is dimensioned such that it fits into transmission case 10 (housing 10 and trapdoor 18) without any modification to the five speed

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transmission case. This is achieved by particular arrangement, shape, and configuration of gears described above, which allows mainshaft 134 to have a bearing region 140 which supports a right mainshaft trapdoor bearing 46 such that the distance between the inside of mainshaft trapdoor bearing 46 is a distance of 5.97 inches from the inside of left mainshaft case bearing 42, which is the same as on a Big Twin five speed transmission. Similarly, the above-described configuration of gears allows the countershaft 144 to have a bearing region 148c which supports a right countershaft trapdoor bearing 48 and a bearing region 148d such that the distance between the inside of countershaft trapdoor bearing 48 and the inside of left countershaft case bearing 44 is also the same as that same distance on a Big Twin five speed transmission. This allows six speed gear set 132 to be installed into a transmission case 10 without any modifications to transmission case 10. Not modifying the transmission case 10 makes the presence of six speed gear set 132 virtually undetectable from a visual inspection of the assembled motorcycle.

Looking next to the shifting assembly 346 by referring primarily to Figures 1 and 2 shifter cam 348, shifter forks 368, 370, and 372, right shift cam support tower 366, and shift cam follower 356 have been modified from their corresponding components of Figure 1A, and are discussed in further detail below. The remainder of the parts for the shifting assembly 346, such as shift fork shaft 120 and left shift cam support tower 110, are the same as the similarly numbered parts of Figure 1A.

Shifter cam 348 is supported by left and right shift cam support towers 110 and 366. The shift grooves 358, 360, and 362 are shown in Figure 2, but, for convenience, have not been accurately depicted in that figure and will be more accurately described further below. Left and right shift cam support towers 110 and 366 are connected to the top of housing 12. Shifter forks 368, 370, and 372 are supported by shift fork shaft 120, which is in turn supported by shift fork shaft support holes 374 and 376.

One end of the 3rd/5th gear shifter fork 368 (Figure 2) engages the 3rd/5th gear shift groove 358 (Figure 6C), and the other end engages fork groove 198 (Figure 3) on mainshaft 1st gear 176. One end of the 1st/2nd gear shifter fork 370 engages the 1st/2nd gear shift groove 360 and the other end engages fork groove 284 on countershaft 3rd gear 280. One end of 4th/6th gear shifter fork 372

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engages the 4th/6th gear shift groove 362 and the other end engages fork groove 246 on the 4th/6th gear shift member 234.

In operation, when the shifter shaft (not shown) rotates in response to the rider operating the shift lever (not shown), the shifter pawl (not shown) acts against the shift pins 364 causing shifter cam 348 to rotate. The rotation of shifter cam 348 causes one or more of shifter forks 368, 370, 372 to move axially along shift fork shaft 120, in turn causing the appropriate gear members to move axially along either mainshaft 134 or countershaft 144, causing a change in the gear ratio. The details of shifter assembly 346 are addressed in more detail below.

Referring now primarily to Figures 7A-7G, these Figures show the necessary axial movements of mainshaft 1st gear 176, countershaft 3rd gear 280, and 4th/6th gear shift member 234 to achieve the available gear ratios of the six speed gear set 132. Figure 7A shows six speed gear set 132 in the neutral position. Namely, none of the dogs of mainshaft 1st gear 176, countershaft 3rd gear 280, or 4th/6th gear shift member 234 are engaging the dog recesses of adjacent gears. Thus, each splined gear is meshing with a freely rotating gear, thereby transmitting no torque.

Referring to Figure 7B, to shift the six speed gear set 132 into 1st gear, countershaft 3rd gear 280 is moved to the left as shown by arrow 386, where left dogs 288 of countershaft 3rd gear 280 will engage the dog recesses 274 of countershaft 1st gear 270. This rotatably couples countershaft 1st gear 270 to the countershaft 144, thus allowing torque to flow as shown by the arrow 388. When six speed gear set 132 is in first gear, it undergoes higher stress than in any other gear. That is why gears 176, 270, 262, and 156 have a wider face width. By placing mainshaft 5th gear 156 and mainshaft 1st gear 176 close to each other and countershaft 5th gear 262 and countershaft 1st gear 270 close to each other, the torque path along countershaft 144 is reduced, thereby resulting in a stronger 1st gear arrangement.

Figure 7C shows that to shift the six speed gear set 132 into 2nd gear, countershaft 3rd gear 280 is moved to the right as shown by arrow 390, where right dogs 292 of countershaft 3rd gear 280 will engage the dog recesses 302 of countershaft 2nd gear 298. This rotatably couples countershaft 2nd gear 298 to the countershaft 144, thus allowing torque to flow as shown by the arrow 392.

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Figure 7D shows that to shift the six speed gear set 132 into 3rd gear, mainshaft 1st gear 176 is moved to the right as shown by arrow 394, where right dogs 194 of mainshaft 1st gear 176 will engage the dog recesses 210 of mainshaft 3rd gear 206. This rotatably couples mainshaft 3rd gear 206 to the mainshaft 134, thus allowing torque to flow as shown by the arrow 396.

Figure 7E shows that to shift the six speed gear set 132 into 4th gear, 4th/6th gear shift member 234 is moved to the left as shown by arrow 398, where left dogs 240 of 4th/6th gear shift member 234 will engage the dog recesses 228 of mainshaft 4th gear 224. This rotatably couples mainshaft 4th gear 224 to the mainshaft 134, thus allowing torque to flow as shown by the arrow 400.

Figure 7F shows that to shift the six speed gear set 132 into 5th gear, mainshaft 1st gear 176 is moved to the left as shown by arrow 402, where left dogs 192 of mainshaft 1st gear 176 will engage the dog recesses 170 of mainshaft 5th gear 156. This rotatably couples mainshaft 5th gear 156 to the mainshaft 134, thus allowing torque to flow as shown by the arrow 404.

Figure 7G shows that to shift the six speed gear set 132 into 6th gear, 4th/6th gear shift member 234 is moved to the right as shown by arrow 406, where right dogs 244 of 4th/6th gear shift member 234 will engage the dog recesses 256 of mainshaft 6th gear 252. This rotatably couples mainshaft 6th gear 252 to the mainshaft 134, thus allowing torque to flow as shown by the arrow 408. Mainshaft 6th gear 252 and countershaft 6th gear 316 are located at opposite sides of transmission case 10. This results in the sixth gear position to have the longest torque path along countershaft 144. Because the least amount of torque is transmitted in sixth gear, this allows shorter torque paths along countershaft 144 for the gear positions that result in higher torque.

Six speed gear set 132, described above, results in the following gear ratios:

<u>Gear</u>	<u>Input:Output Ratio</u>
1st gear	2.94:1
1st gear (alt.)	3.21:1
2nd gear	2.082:1
3rd gear	1.531:1
4th gear	1.242:1



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5th gear	1.00:1
6th gear	0.893:1
6th gear (alt.)	0.860:1

5 The above gear ratios are measured with the input being the rotation of mainshaft 134 and the output being the rotation of mainshaft 5th gear 156.

Referring now to Figures 6A-6C, the details of shifter cam 348 are seen in more detail. Figure 6A shows a view of shifter cam 348 taken along line 6A-6A of Figure 2A. Figure 6B shows a view of shifter cam 348 taken along line 6B-6B of Figure 2A and showing the arrangement of pins 364. Figure 6C is a flattened depiction of the cylindrical surface of shifter cam 348, including the shift grooves 358, 360, and 362. The line labeled "1st" in Figure 6C matches with the zero degree cam lead angle of Figure 6A, and the remainder of Figure 6C "wraps" clockwise around shifter cam 348. Valleys 350a-350g, in conjunction with shift cam follower 356 bias shifter cam 348 to one of seven predetermined positions.

15 When shift cam follower 356 is at valley 350g, shift forks 386, 370, and 372 are along line "N" of Figure 6C, and mainshaft 1st gear 176, countershaft 3rd gear 280, and 4th/6th gear shift member 234 are not engaging any adjacent gears, thus causing six speed gear set 132 to be in the configuration of Figure 7A — the neutral position.

20 When shift cam follower 356 is at valley 350a, shift forks 368, 370, and 372 are along line "1st" of Figure 6C, and 1st/2nd gear shift groove 360 will cause 1st/2nd gear shifter fork 370 to move countershaft 3rd gear 280 to the left, thus causing six speed gear set 132 to be in the configuration of Figure 7B — first gear.

25 When shift cam follower 356 is at valley 350b, shift forks 368, 370, and 372 are along line "2nd" of Figure 6C, and 1st/2nd gear shift groove 360 will cause 1st/2nd gear shifter fork 370 to move countershaft 3rd gear 280 to the right, thus causing six speed gear set 132 to be in the configuration of Figure 7C — second gear.

30 Similarly, when cam follower 356 is at valleys 350c, 350d, 350e, and 350f, shift forks 368, 370, and 372 will be along lines "3rd", "4th", "5th", and "6th", respectively, thus causing the appropriate movement of mainshaft 1st gear 176, countershaft 3rd gear 280, and/or 4th/6th gear shift member 234 to place six speed

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gear set 132 into third, fourth, fifth, and sixth speeds, respectively.

Referring now particularly to Figure 6A, the particular spacing and shape of the peaks and valleys of the cam surface followed by the shift cam follower 356 is shown. Valleys 350a-350f are evenly spaced at  $60^{\circ}$  apart from each other. Also, each valley 350a-350f has a radius of 0.125 inches, each peak 352b-352f has a radius of 0.25 inches, and the ramps leading from each valley to the two adjacent peaks form an angle of  $120^{\circ}$  (for example see the angle labeled 354). Peaks 352a' and 352a" and valley 350g are the exception in that valley 350g corresponds to the neutral position and was placed between otherwise equally spaced-apart valleys. The uniformity in the spacing and shape of the valleys 350a-350f and peaks 352b-352f, and the particular angle of the ramps between valleys 350a-350f and peaks 352b-352f results in smoother, more uniform shifting with a shift lever throw that is the same in every gear. Also, it allows the shift pawl to be adjusted when the gears are in any one of several configurations (e.g. 2nd gear, 3rd gear, 4th gear, and 5th gear).

To convert a Big Twin five speed transmission into a six speed transmission using the present invention, the only parts of the five speed transmission that need to be replaced are mainshaft 62, countershaft 64, mainshaft 5th gear 66, mainshaft 2nd gear 68, mainshaft 3rd gear 70, mainshaft 1st gear 72, mainshaft 4th gear 74, countershaft 5th gear 76, countershaft 2nd gear 78, countershaft 3rd gear 80, countershaft 1st gear 82, countershaft 4th gear 84, shifter cam 96, right shift cam support tower 112, shift cam follower 108, shift fork 114, shift fork 116, shift fork 118, and the split case bearings, retaining rings, thrust washers, and spacers.

While the invention has been particularly shown and described with reference to a preferred embodiment, it will be understood by those skilled in the art that various changes in form and detail may be made therein without departing from the spirit and scope of the invention.

Claims

1. A method of converting a five speed motorcycle transmission of the type having an original transmission housing with left and right side walls, an original driveshaft supported at the right and left side walls by bearings at opposite ends of the original driveshaft, the bearings being separated by a bearing-to-bearing distance, the original driveshaft having an end portion extending outwardly from the original transmission housing beyond the left side wall, the end portion being adapted to be rotatably coupled to an output from a motorcycle engine, an original countershaft mounted in the original transmission housing in horizontally spaced parallel relationship to the original driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall, an output sprocket mounting member concentrically disposed about the driveshaft end portion located outside the original transmission housing, the output sprocket mounting member being rigidly connected to a gear inside the original transmission housing, five original driveshaft gears disposed about the original driveshaft and five original countershaft gears disposed about the original countershaft, the original driveshaft gears and the original countershaft gears being selectively positionable to selectively provide any one of five drive ratios and an idle ratio, into a six speed transmission, the method comprising the steps of:
- 20 leaving the original transmission housing mounted on a motorcycle;  
opening the original transmission housing;  
removing the original driveshaft, original countershaft, original five driveshaft gears, and original five countershaft gears from the original transmission housing;  
replacing the original driveshaft with a replacement driveshaft adapted to receive six replacement gears and being mountable within the original transmission housing;  
25 replacing the original countershaft with a replacement countershaft adapted to receive six replacement countershaft gears and being mountable within the original transmission housing;  
30 placing six replacement driveshaft gears about the replacement driveshaft;  
placing six replacement countershaft gears about the replacement countershaft;

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positioning the replacement mainshaft, replacement countershaft, and replacement gears within the original transmission housing; and

closing the original transmission housing wherein the five speed motorcycle transmission is converted to a six speed motorcycle transmission without modifying the housing.

2. The method of claim 1 wherein the six replacement driveshaft gears and the six replacement countershaft gears are selected and placed such that the output sprocket mounting member rotates faster than the driveshaft in at least one drive ratio, thus providing an overdrive ratio.

3. The method of claim 1 wherein the five speed transmission is selected to be a non-overdrive transmission such that in any drive ratio the output sprocket mounting member rotates no faster than the driveshaft, and wherein the replacement driveshaft gears and replacement countershaft gears are selected such that the output sprocket mounting member rotates faster than the driveshaft in at least one drive ratio, thus providing an overdrive ratio.

4. A motorcycle transmission of the type having a transmission housing with left and right side walls, a driveshaft supported at the right and left side walls by bearings at opposite ends of the driveshaft, the bearings being separated by a bearing-to-bearing distance, the driveshaft having an end portion extending outwardly from the transmission housing beyond the left side wall, the end portion being adapted to be rotatably coupled to an output from a motorcycle engine, a countershaft mounted in the transmission housing in horizontally spaced parallel relationship to the original driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall, an output sprocket mounting member concentrically disposed about the driveshaft end portion located outside the transmission housing, the output sprocket mounting member being rigidly connected to a gear inside the transmission housing, the motorcycle transmission comprising:

six driveshaft gears disposed about the driveshaft;

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six countershaft gears disposed about the countershaft;  
the driveshaft gears and countershaft gears being selectively positionable to selectively provide any one of six drive ratios and an idle ratio.

5        5.        The motorcycle transmission of claim 4 wherein the bearing-to-bearing distance is the same as a bearing-to-bearing distance on five speed transmissions on Harley-Davidson Big Twin motorcycles.

10       6.        The motorcycle transmission of claim 4 wherein the bearing-to-bearing distance is 5.97 inches.

15       7.        The motorcycle transmission of claim 4 wherein at least one of the six drive ratios causes the output sprocket mounting member to rotate faster than the driveshaft, resulting in an overdrive ratio.

20       8.        A motorcycle transmission gear assembly for motorcycles with transmissions of the type having a transmission housing with left and right side walls, a driveshaft supported at the right and left side walls by bearings at opposite ends of the driveshaft, the bearings being separated by a bearing-to-bearing distance, the driveshaft having an end portion extending outwardly from the transmission housing beyond the left side wall, the end portion being adapted to be rotatably coupled to an output from a motorcycle engine, a countershaft mounted in the transmission housing in horizontally spaced parallel relationship to the original driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall, an output sprocket mounting member concentrically disposed about the driveshaft end portion located outside the transmission housing, the output sprocket mounting member being rigidly connected to a driveshaft drive gear inside the transmission housing, the motorcycle transmission gear assembly comprising:

30            the driveshaft drive gear;  
             a driveshaft overdrive gear;  
             a countershaft overdrive gear;

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a countershaft drive gear;

the gear assembly being adapted to fit inside the housing of a non-overdrive Harley-Davidson Big Twin transmission housing;

the gear assembly being arranged such that in the drive ratio which utilizes the driveshaft drive gear, the driveshaft overdrive gear, the countershaft overdrive gear, and the countershaft drive gear, the input torque from the driveshaft is transferred along the driveshaft, to the driveshaft overdrive gear, to the countershaft overdrive gear, along the countershaft, to the countershaft drive gear, to the driveshaft drive gear, and to the output sprocket mounting member in such a way that the output sprocket mounting member turns faster than the driveshaft, thus providing an overdrive ratio.

9. The motorcycle transmission of claim 8 wherein the bearing-to-bearing distance is the same as a bearing-to-bearing distance on five speed transmissions on Harley-Davidson Big Twin motorcycles.

10. The motorcycle transmission of claim 8 wherein the bearing-to-bearing distance is 5.97 inches.

11. An improved transmission system for a motorcycle, the transmission system having a mode of operation which comprises:

a housing defined by left and right side walls;

a driveshaft mounted in the housing with a right end rotatably mounted in the right side wall and a left end rotatably mounted in the left side wall and having an end portion extending outwardly from the housing beyond the left side wall, the end portion being adapted for rotational coupling to an output from an engine of the motorcycle;

a countershaft mounted in the housing in horizontally spaced parallel relationship to the driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall;

a driveshaft drive gear freely rotatably mounted on the driveshaft inside the housing and immediately adjacent the left side wall;

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an output sprocket mounting member located outside the housing and rigidly connected to the driveshaft drive gear;

a driveshaft overdrive gear mounted on and rotatably coupled to the driveshaft inside the housing and immediately adjacent the right side wall;

5        a countershaft overdrive gear mounted on the countershaft and rotatably coupled thereto;

the driveshaft overdrive gear and the countershaft overdrive gear being in meshing engagement;

10       a countershaft drive gear mounted on the countershaft and rotatably coupled thereto;

the countershaft drive gear and the driveshaft drive gear being in meshing engagement;

15       wherein input torque to the driveshaft is transferred along the driveshaft, to the engagement member, to the driveshaft overdrive gear, to the countershaft overdrive gear, along the countershaft, to the countershaft drive gear, to the driveshaft drive gear, and to the output sprocket mounting member, and wherein the output sprocket mounting member rotates faster than the driveshaft.

20       12. The improved transmission system of claim 11 wherein a mainshaft first gear is located adjacent the driveshaft drive gear and a countershaft first gear is located adjacent the countershaft drive gear.

25       13. The improved transmission system of claim 11 wherein a mainshaft first gear is located adjacent the driveshaft drive gear and a countershaft first gear is located adjacent the countershaft drive gear, a mainshaft third gear is located adjacent the mainshaft first gear and a countershaft third gear is located adjacent the countershaft first gear, a mainshaft second gear is located adjacent the mainshaft third gear and a countershaft second gear is located adjacent the countershaft third gear, a mainshaft fourth gear is located adjacent the mainshaft second gear and a  
30       countershaft fourth gear is located adjacent the countershaft second gear.

14. An improved motorcycle transmission system having a mode of operation

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which comprises:

a housing defined by left and right side walls;

a driveshaft mounted in the housing with a right end rotatably mounted in the right side wall and a left end rotatably mounted in the left side wall and having an end portion extending outwardly from the housing beyond the left side wall;

a countershaft mounted in the housing in horizontally spaced parallel relationship to the driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall;

a driveshaft drive gear freely rotatably mounted on the driveshaft inside the housing and immediately adjacent the left side wall;

an output sprocket mounting member located outside the housing and rigidly connected to the driveshaft drive gear;

a driveshaft first gear mounted on and rotatably coupled to the driveshaft immediately adjacent the driveshaft drive gear;

a countershaft first gear mounted on and rotatably coupled to the countershaft;

the driveshaft first gear and the countershaft first gear being in meshing engagement;

a countershaft drive gear mounted on the countershaft and rotatably coupled thereto;

the countershaft drive gear and the driveshaft drive gear being in meshing engagement;

wherein input torque to the driveshaft is transferred along the driveshaft, to the driveshaft first gear, to the countershaft first gear, along the countershaft, to the countershaft drive gear, to the driveshaft drive gear, and to the output sprocket mounting member with a predetermined drive ratio which has greatest difference between a rotational velocity of the output sprocket mounting member and a rotational velocity of the driveshaft compared to other drive ratios provided by the transmission system.

15. The improved motorcycle transmission system of claim 14 wherein:

the driveshaft drive gear has a right side adjacent the driveshaft first gear, and



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a recess in said right side;

said recess adapted to receive the driveshaft first gear wherein in another mode of operation a toothed portion of the driveshaft first gear fits at least partially inside the driveshaft drive gear.

16. A gear for a motorcycle transmission gear assembly, the gear comprising:  
a gear body having a central portion located between a left and right end portions and adapted to rotate about a longitudinal axis;

external gear teeth disposed about the circumference of the central portion;

a left flange extending radially from the left end portion;

left lugs extending longitudinally from the left flange and away from the gear body;

a right flange extending radially from the right end portion;

right lugs extending longitudinally from the right flange and away from the gear body;

a left annular groove defined between the gear teeth and the left flange;

a right annular groove defined between the gear teeth and the right flange.

17. The gear of claim 16 wherein the gear is a mainshaft first gear.

18. The gear of claim 16 wherein the left and right annular grooves have a depth extending to the root of the gear teeth.

19. The gear of claim 16 wherein one of the annular grooves is a fork groove.

20. The gear of claim 16 wherein the gear is adapted to be assembled immediately adjacent a driveshaft drive gear.

21. The gear of claim 16 wherein the gear is adapted to be assembled immediately adjacent a driveshaft drive gear having a recess and wherein the gear of claim 16 is adapted so that at least a part of the central portion having teeth can fit within a recess of the driveshaft drive gear in at least one mode of operation.

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22. A motorcycle transmission of the type having a transmission housing with left and right side walls, a driveshaft mounted in the housing with a right end rotatably mounted in the right side wall and a left end rotatably mounted in the left side wall and having an end portion extending outwardly from the housing beyond the left side wall, the end portion being adapted to be rotatably coupled to an output from a motorcycle engine, a countershaft mounted in the housing in horizontally spaced parallel relationship to the driveshaft and with a right end rotatably mounted to the right side wall and a left end rotatably mounted to the left side wall, an output sprocket mounting member concentrically disposed about the driveshaft end portion located outside the housing, the output sprocket mounting member being rigidly connected to a gear inside the transmission housing, the gear assembly comprising:

- a plurality of driveshaft gears disposed about the driveshaft;

- a plurality of countershaft gears disposed about the countershaft;

- the driveshaft gears and the countershaft gears being selectively movable into a plurality of arrangements that result in a plurality of drive ratios for the transmission;

- a shifter cam member rotatably mounted in the housing in spaced parallel relationship to the driveshaft and the countershaft;

- the shifter cam member having a plurality of shifter grooves that allow a plurality of shifter forks to be moved sideways in a direction parallel to the driveshaft and countershaft;

- the shifter cam member having a cam surface with a plurality of valleys adapted to engage a cam follower which biases the shifter cam member to one of a plurality of positions, each position corresponding to a particular drive ratio;

- the valleys of the cam surface of the shifter cam member being evenly spaced around the shifter cam member;

- wherein a shift pawl can be adjusted when the gears are in more than one configuration.

23. The motorcycle transmission of claim 22 wherein the valleys corresponding to non-neutral gear ratios are spaced 60 degrees one from the other, allowing smoother and more uniform shifting.

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24. The motorcycle transmission of claim 22 wherein the valleys corresponding to non-neutral gear ratios are formed by ramps forming an angle of 120 degrees, allowing smoother and more uniform shifting.

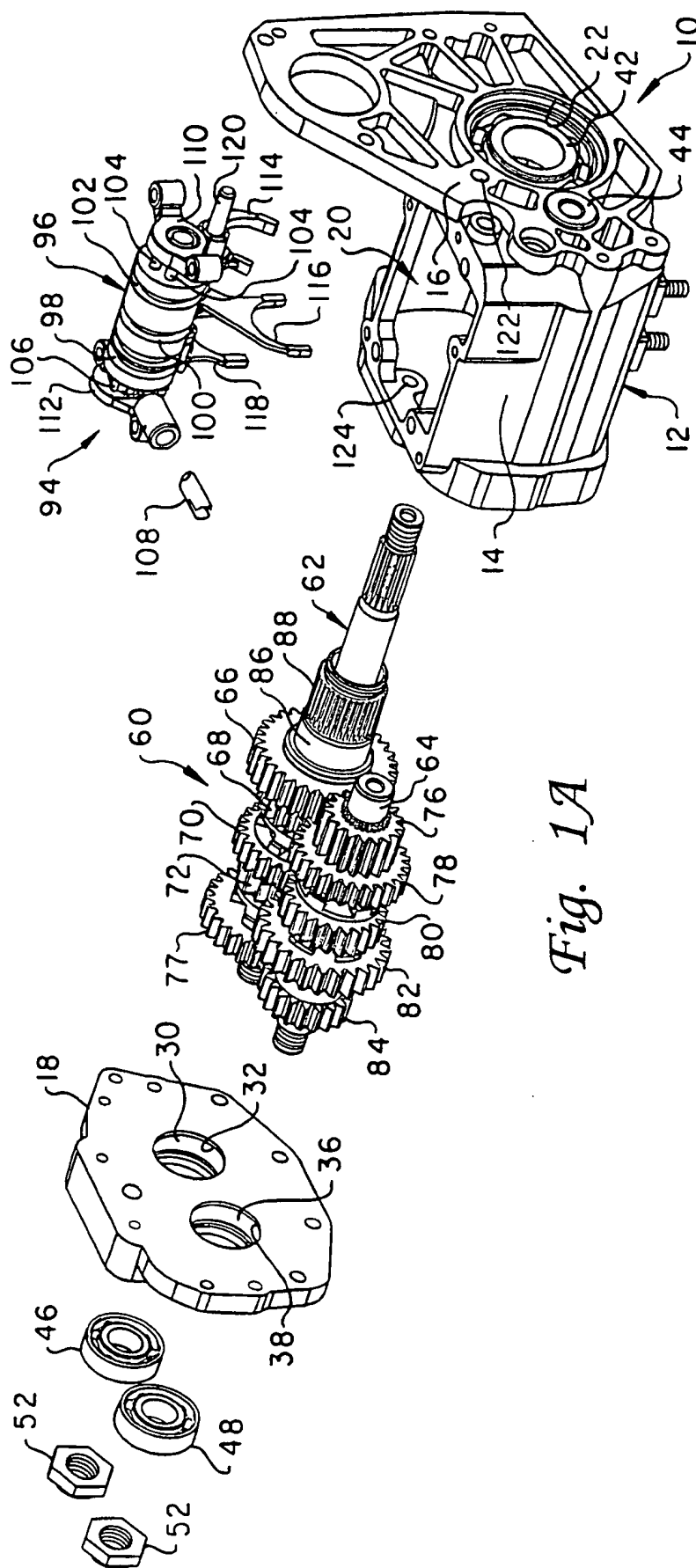


Fig. 1A

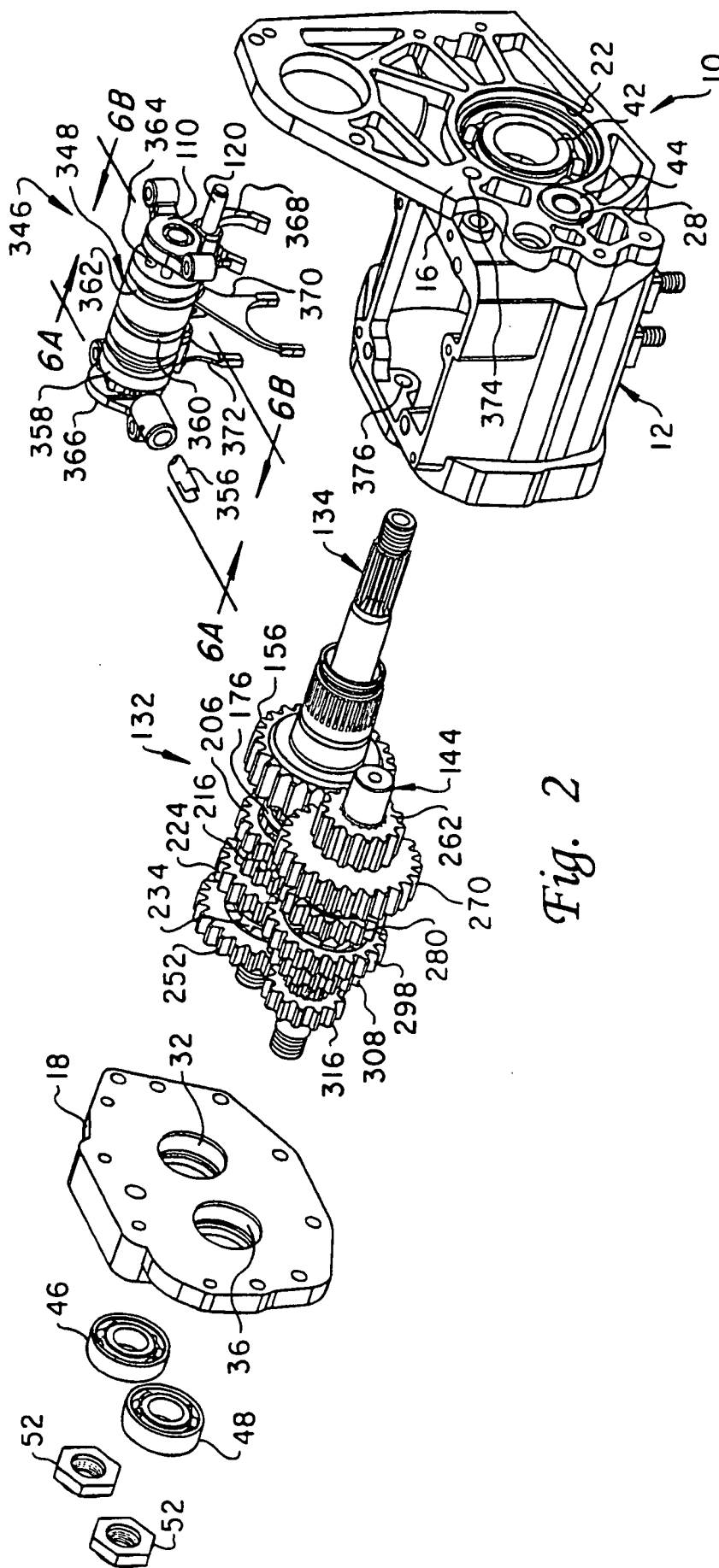


Fig. 2

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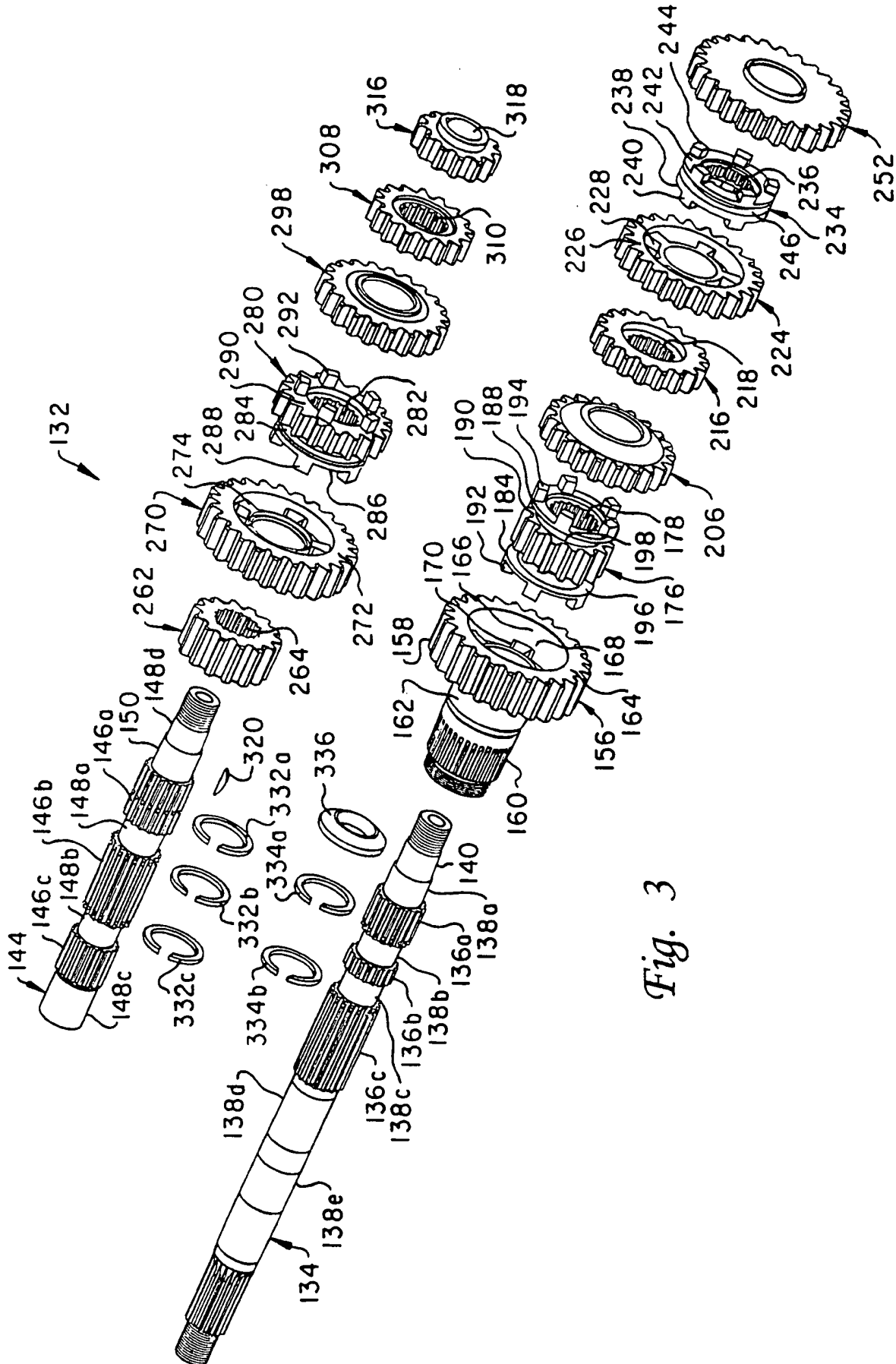


Fig. 3

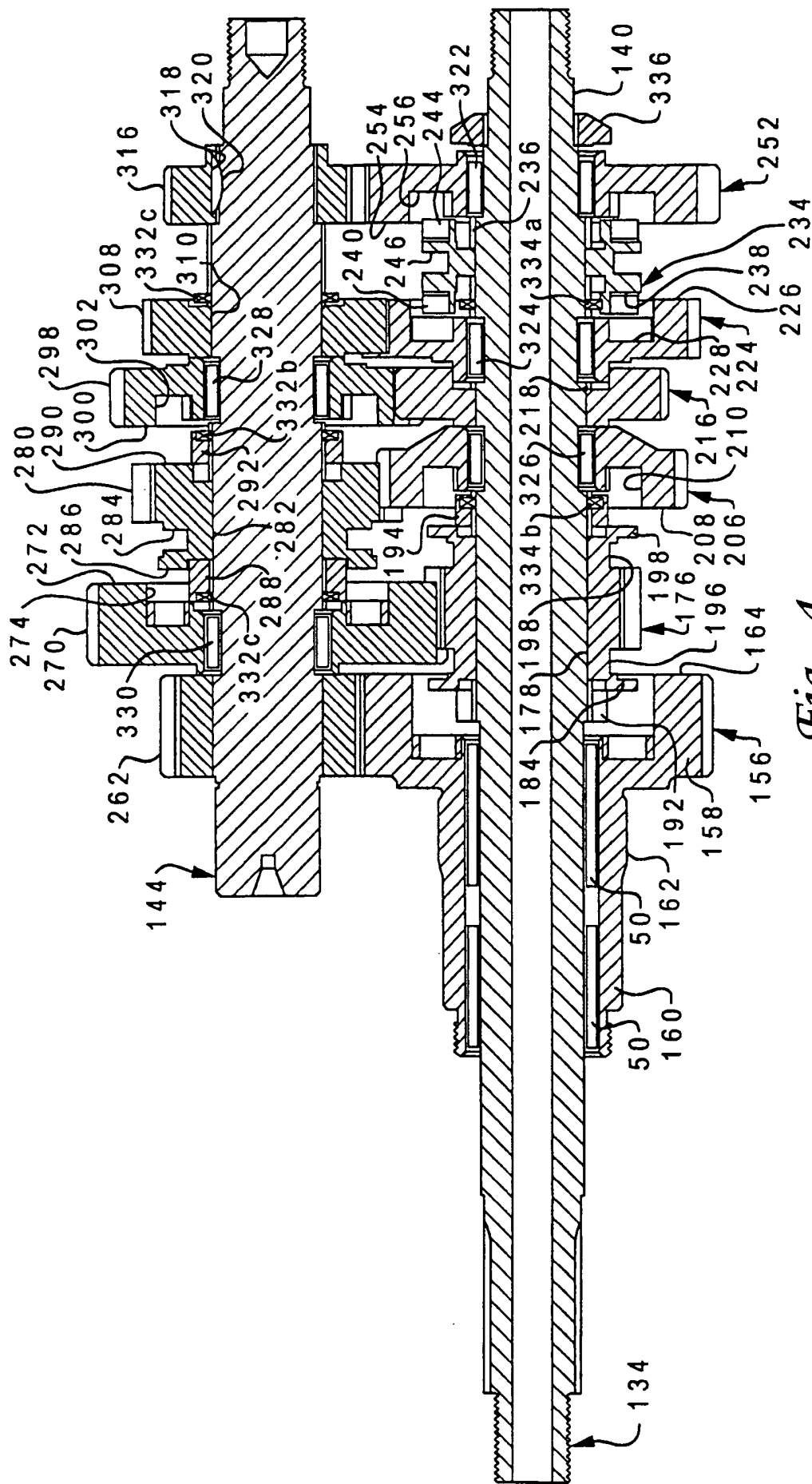


Fig. 4

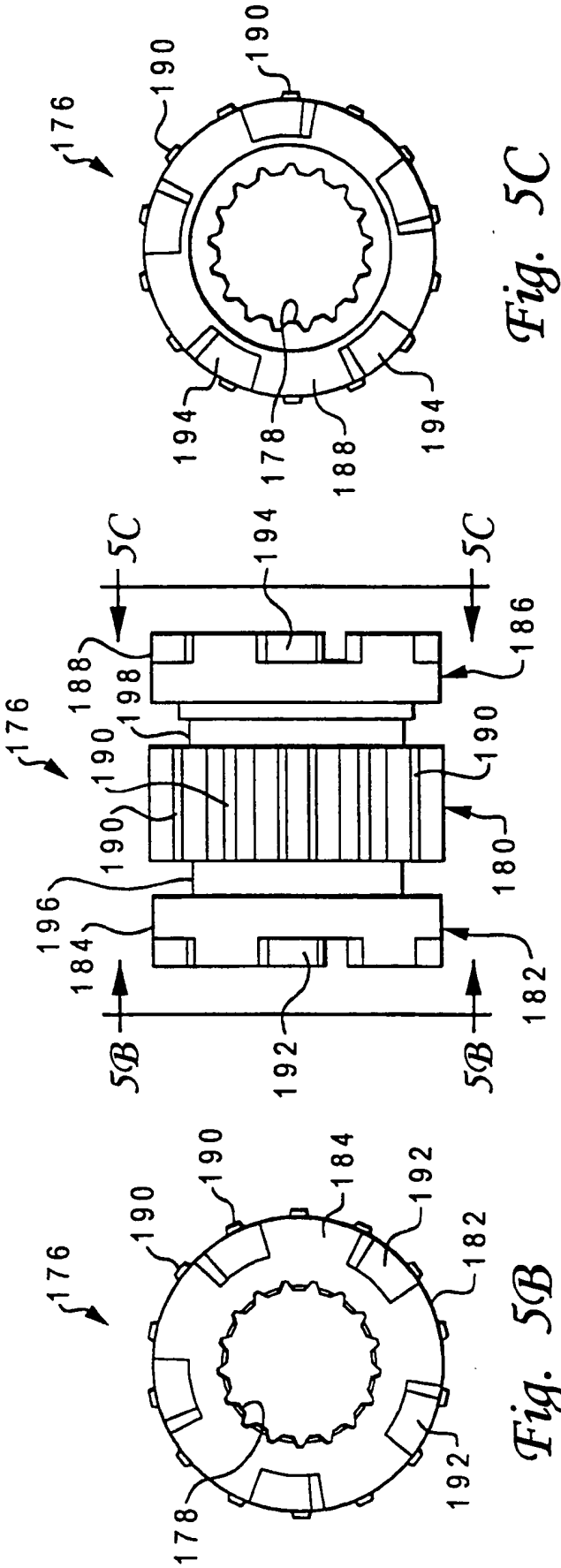


Fig. 5C

Fig. 5A

Fig. 5B



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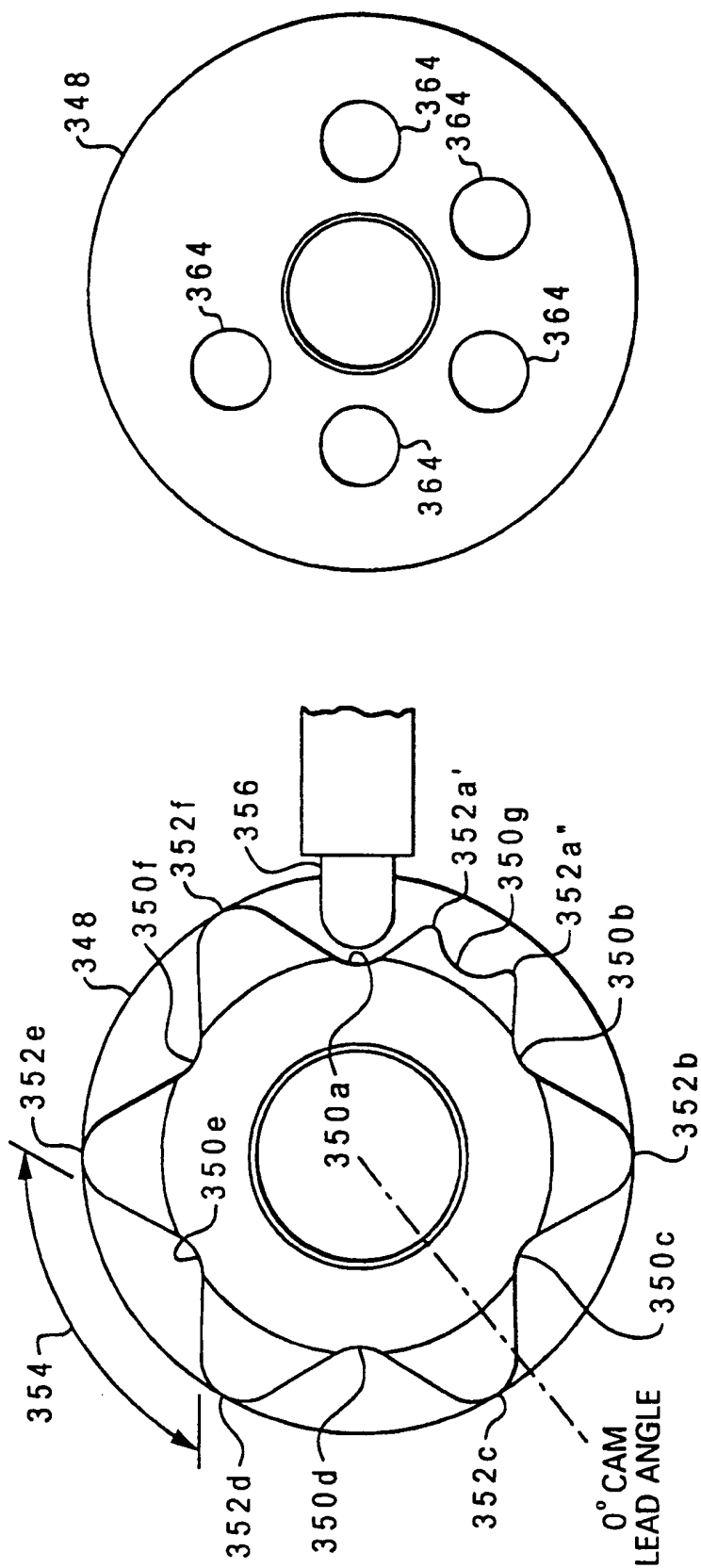
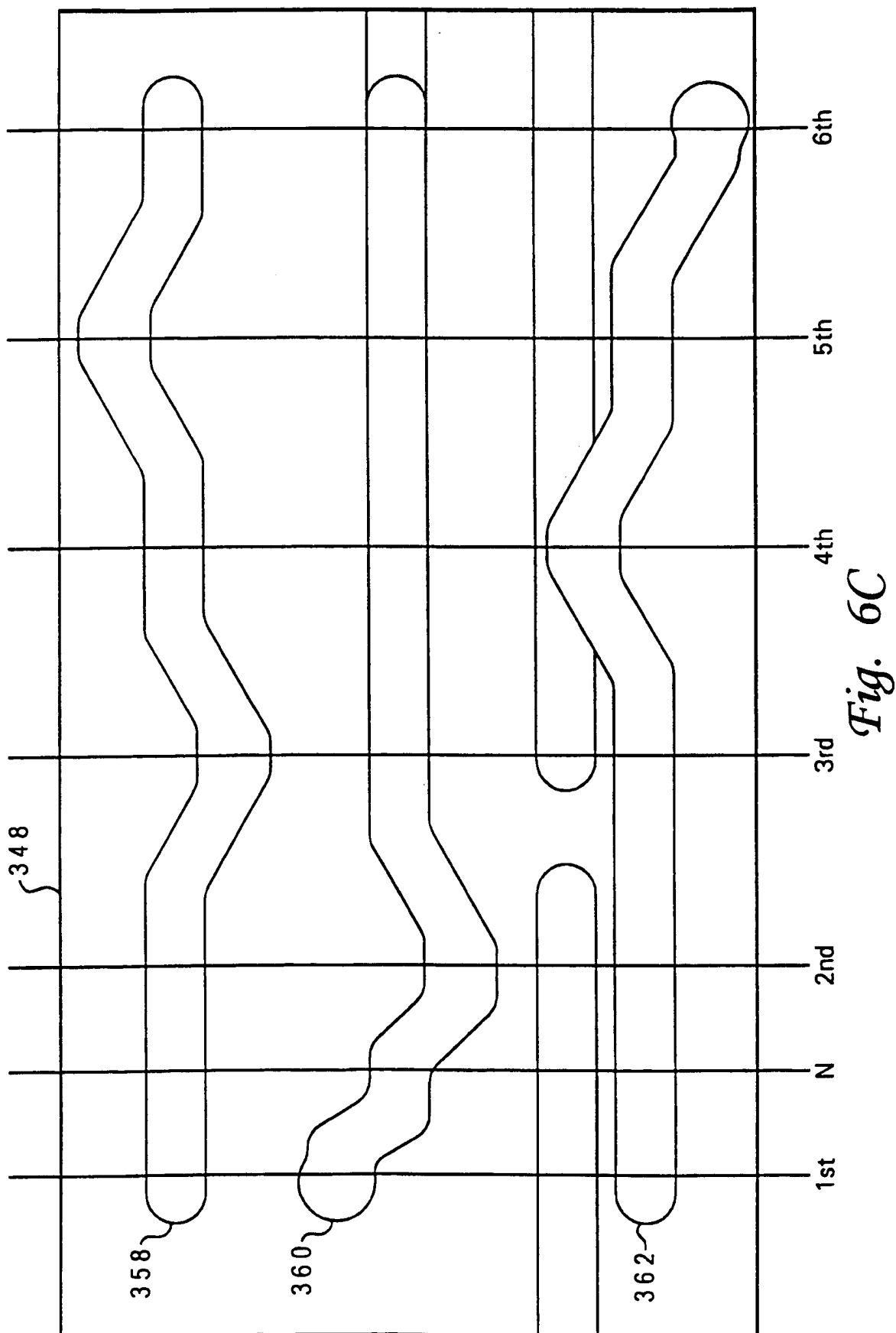


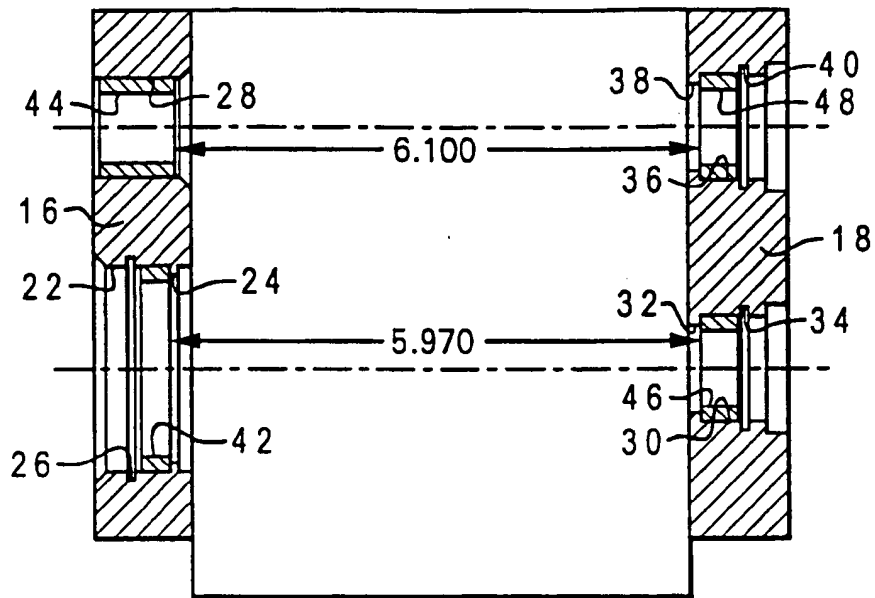
Fig. 6B

Fig. 6A

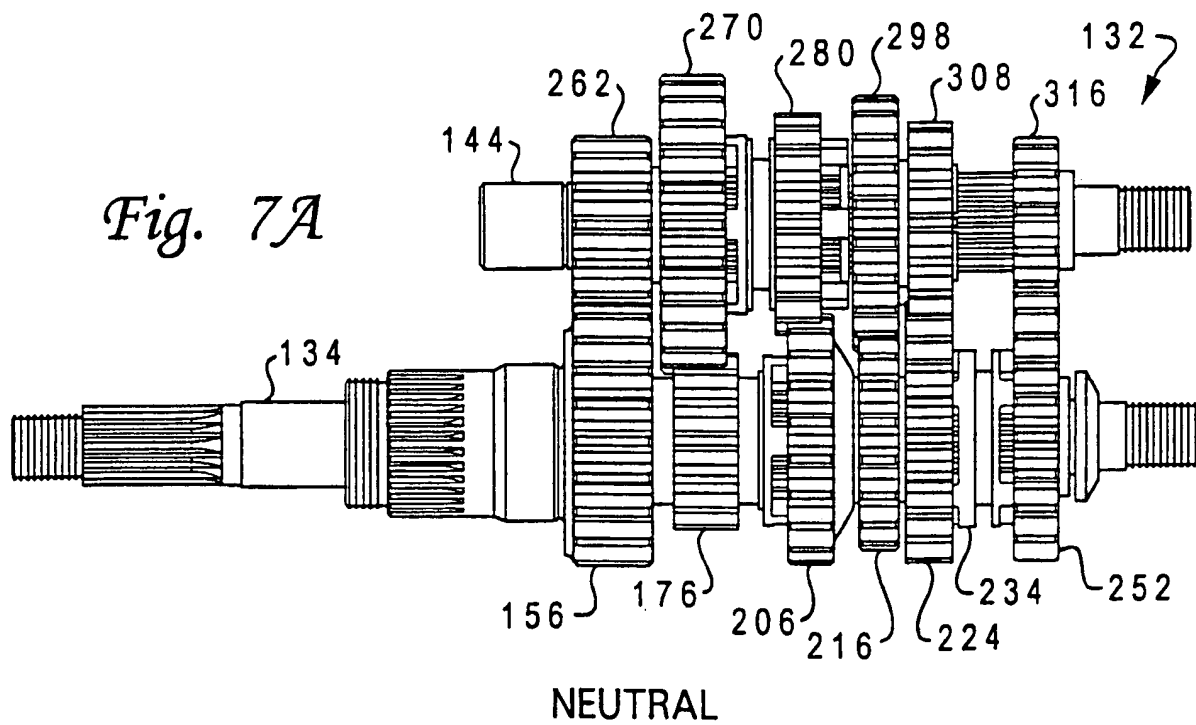
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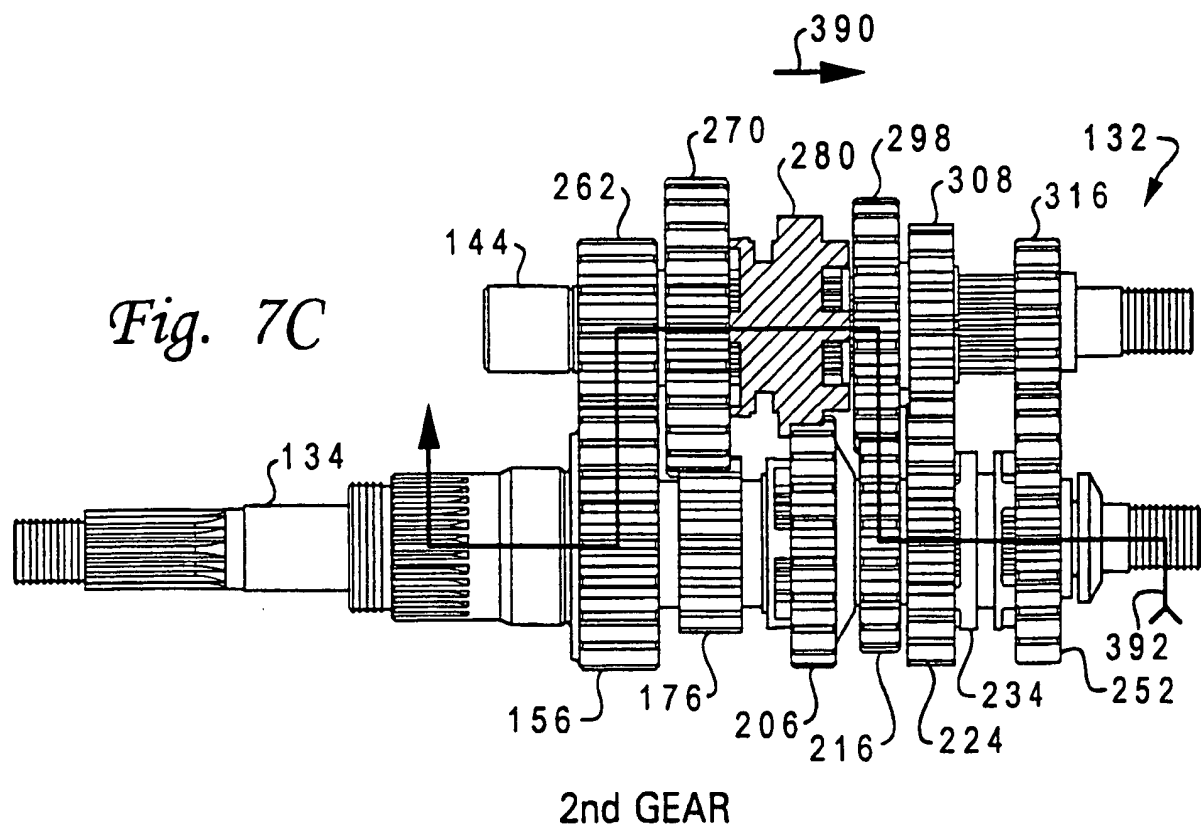
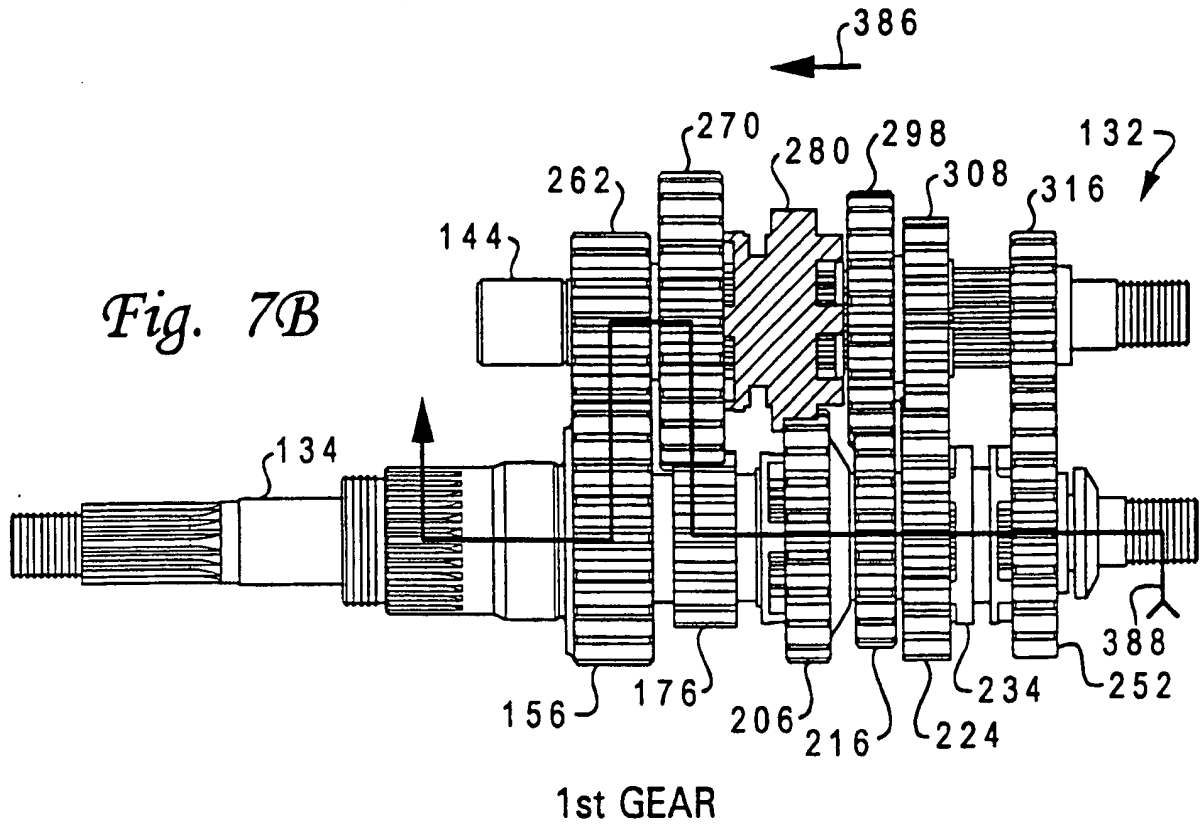
*Fig. 1B*  
*Prior Art*



*Fig. 7A*

NEUTRAL

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Fig. 7D

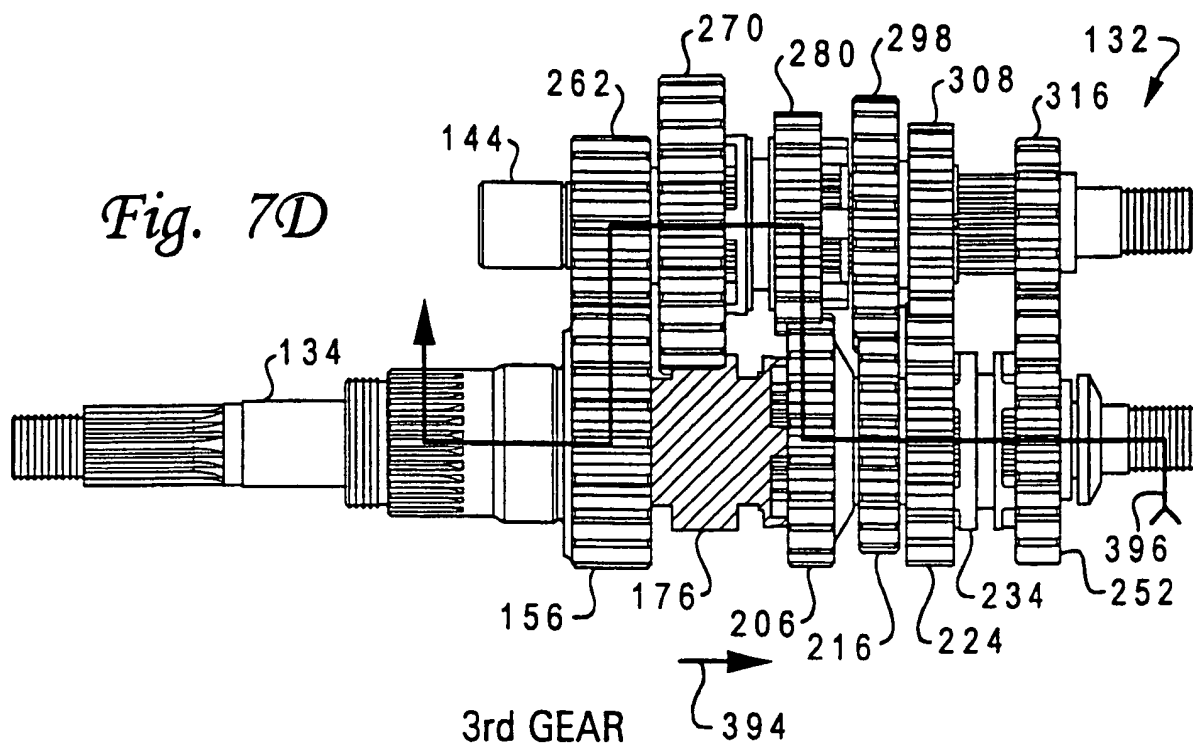
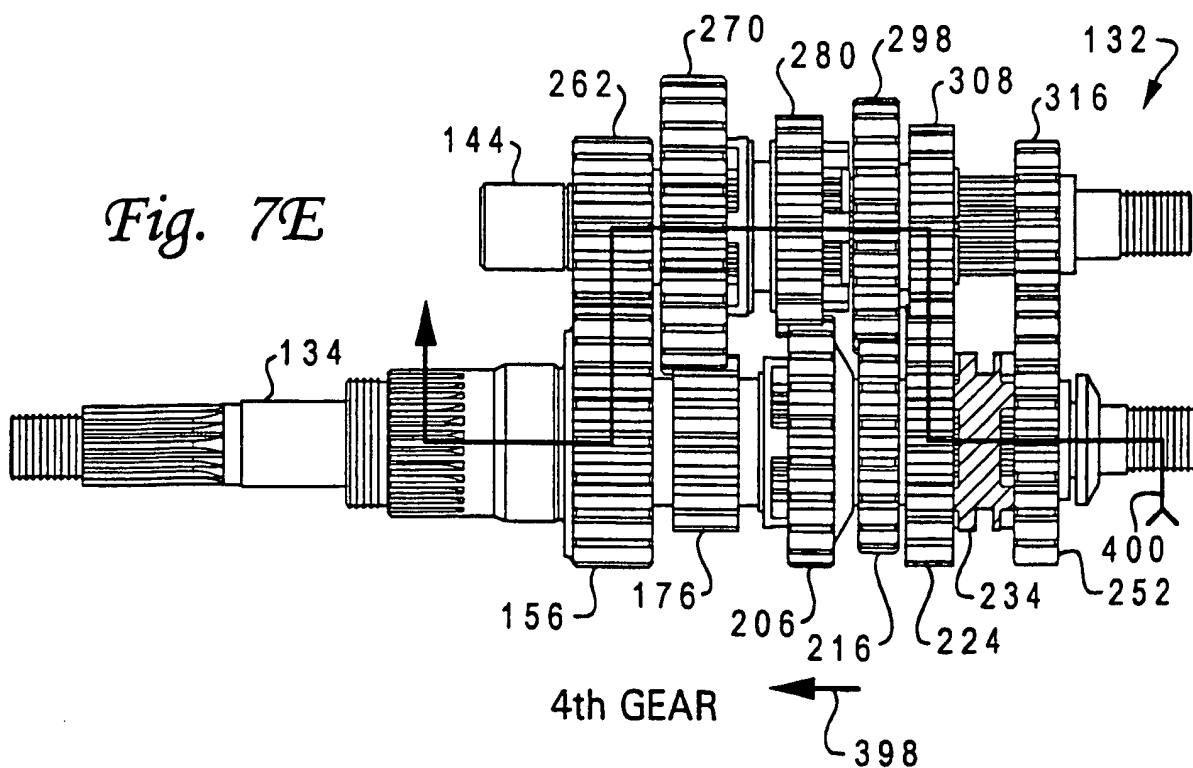
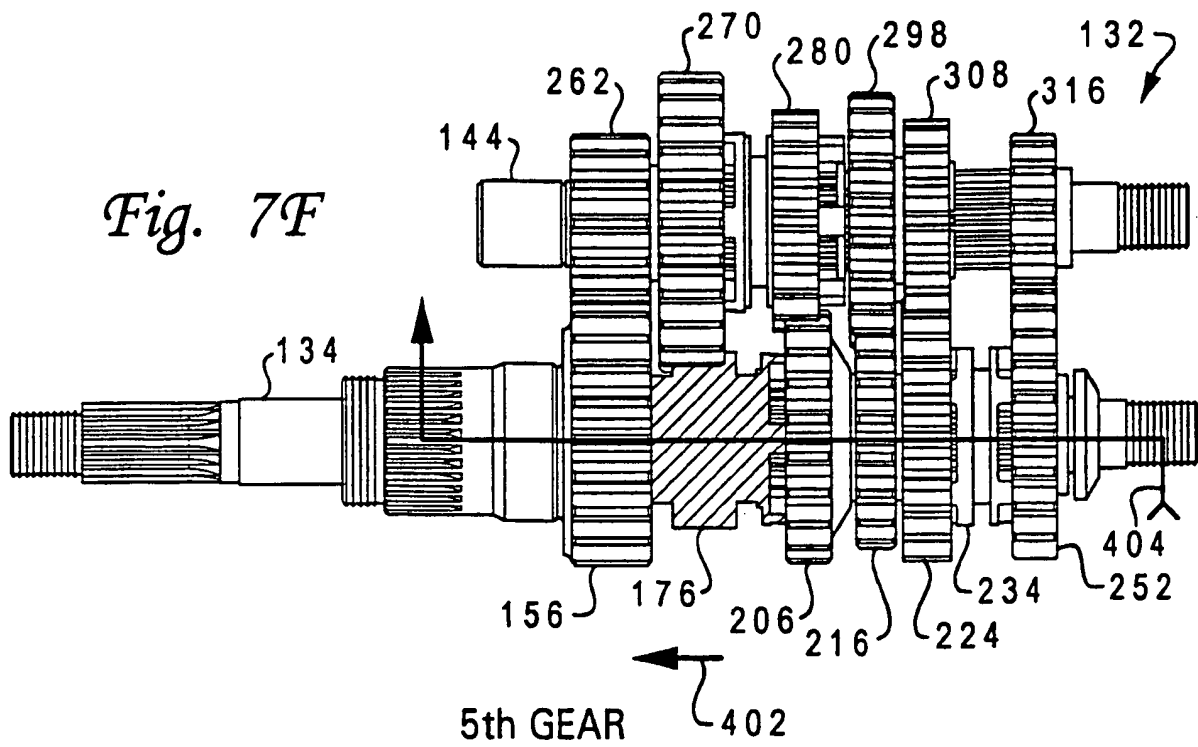


Fig. 7E

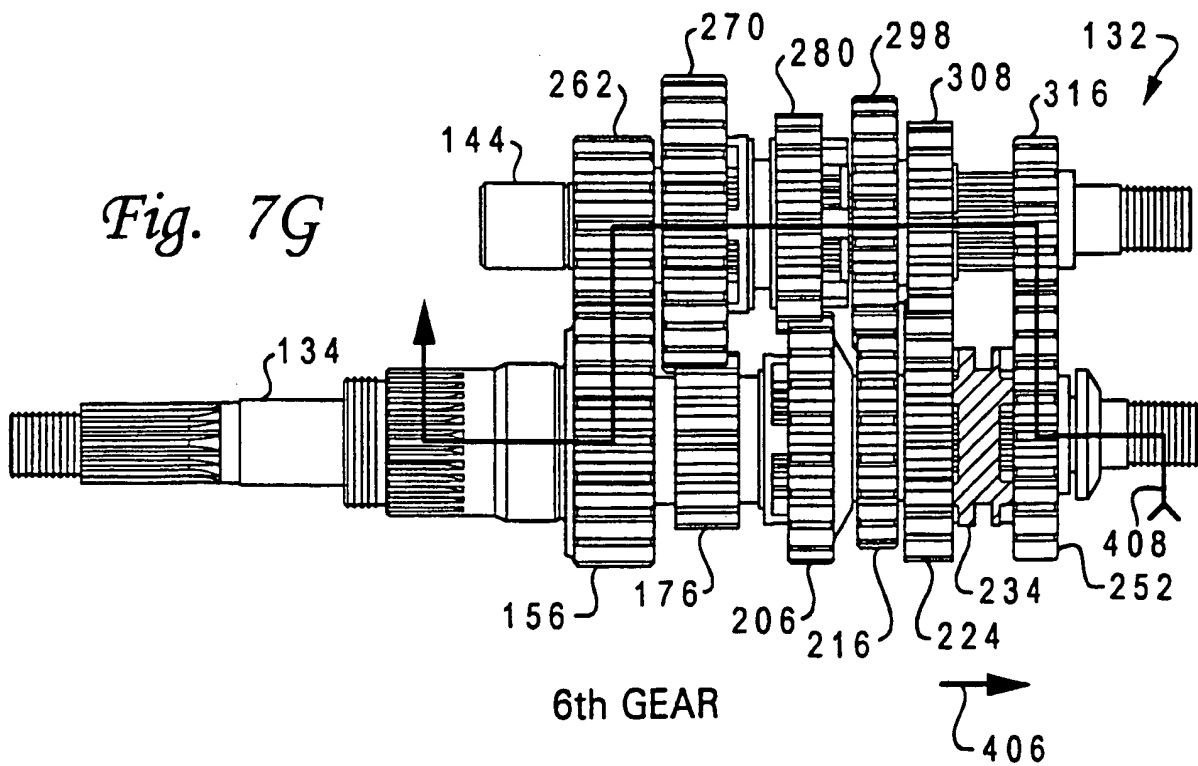


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*Fig. 7F*



*Fig. 7G*



# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 99/13350

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 F16H3/091 F16H63/14 F16H55/17

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 F16H F16D B23F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 079 176 A (SECR DEFENCE BRIT) 18 May 1983 (1983-05-18) abstract figure 2	14, 15
A	---	4, 8, 11, 12, 22, 23
X	GB 208 370 A (ALLTREE ARTHUR) 20 December 1923 (1923-12-20) page 3, line 11 - line 28 page 3, line 101 - line 107 figures 1-3	22, 23
A	---	1, 4, 8, 11
	US 4 157 044 A (PELTZ JOHNNY W) 5 June 1979 (1979-06-05) the whole document ---	
	-/--	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents:

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

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Date of the actual completion of the international search

1 February 2000

Date of mailing of the international search report

15.03.00

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Wilson, M

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 99/13350

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 606 310 A (MAKINO SAKAE) 19 August 1986 (1986-08-19) abstract figure 3 ---	1,4
A	US 4 373 601 A (ONDA TAKANORI ET AL) 15 February 1983 (1983-02-15) abstract column 1, line 17 - line 37 figures 1,2 ---	1,8
A	US 2 316 477 A (WEAVER GEORGE B) 13 April 1943 (1943-04-13) page 1, line 6 - line 10 page 2, line 63 - line 87 figure 4 ---	4,8,11
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